

→ FSBPA Technical Conference

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Curry Hammock Park Tidal Restoration

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Agenda

- Project Background and Team
- Hydrodynamic Model Development
 - Model Domain
 - Boundary Conditions and Forcing
 - Calibration
- Selection of Design Neap Period
- Tidal Improvement Scenario Results
 - Tidal Flushing Analysis
 - Sedimentation
 - Structure flushing analysis
 - Sedimentation patterns



Project Background

- Curry Hammock State Park is located along U.S. Highway 1/Overseas Highway in Marathon, FL (Monroe County).
- During the development of this area the historical tidal connections between the FL Bay and the Atlantic Ocean were filled.
- The tidal restoration aims to re-establish the surface water connection to improve circulation and flushing.



Project Team



Florida Department of Environmental Protection (FDEP) – Project Sponsor



Gresham Smith Prime, Roadway/MOT, Structural



ESA Environmental, Permitting



GHD Hydraulics



Terracon Geotech

GPI Survey



Structural



DRMP SUE

Model Domain



- Regional domain covering
 Florida-Bahamas-Cuba area
- Unstructured (triangular) mesh containing 66,850 nodes and 119,614 elements

Model Domain - Local



Boundary Conditions



- Boundary Conditions:
 - Water Current Velocities and Water Surface Elevations
 - Combined Global HYCOM + DHI Tidal model
- Meteorological Forcing
 - Spatially and Temporally Varying Wind Speeds
 - ERA 5 Global Wind Fields

Model Calibration



- Three (3) Water Surface Elevation (WSE) stations
- One (1) Current Velocity station
- Calibration period:
 - March/April 2013 to align with current velocity data timeframe

Model Calibration - WSE

| Station | MAE (m) | IOA (-) | | |
|------------------|---------|---------|--|--|
| Key Colony Beach | 0.08 | 0.94 | | |
| Key West | 0.10 | 0.88 | | |
| Vaca Key | 0.12 | 0.50 | | |

MAE: Mean Absolute Error.

IOA: Indices of Agreement. Values >0.5 indicate good model calibration, values close to 1 represent excellent calibration per Wilmott et al. (1985)





Model Calibration - Currents

| Station | MAE (m/s) | IOA (-) | | |
|---------------|-----------|---------|--|--|
| Moser Channel | 0.17 | 0.70 | | |

MAE: Mean Absolute Error.

IOA: Indices of Agreement. Values >0.5 indicate good model calibration, values close to 1 represent excellent calibration per Wilmott et al. (1985)





Selection of Design Neap Period





| Rank | Date | Tidal Range (m) | | |
|------|----------|-----------------|--|--|
| 1 | 11/15/10 | 0.34 | | |
| 2 | 1/3/20 | 0.346 | | |
| 3 | 5/7/10 | 0.349 | | |
| 4 | 12/5/19 | 0.351 | | |
| 5 | 5/8/10 | 0.353 | | |
| 6 | 12/13/10 | 0.357 | | |
| 7 | 11/16/14 | 0.358 | | |
| 8 | 5/8/14 | 0.359 | | |
| 9 | 5/29/23 | 0.359 | | |
| 10 | 5/28/23 | 0.36 | | |

Tidal Improvement Scenarios

Figure 2 – Proposed Culvert Locations



<u>Scenario 1</u>: 10' x 10' **Triple** Box Culvert at Both East & West Locations

<u>Scenario 2</u>: 10' x 10' **Double** Box Culvert at Both East & West Locations

Tidal Improvement Scenarios



Scenario 3: 10' x 10' Triple Box Culvert at West Location & 10' x 10' Double Box Culvert at East Location

Scenario 4: 10' x 8' Triple Box Culvert at West Location & 10' x 8' Double Box Culvert at East Location

Scenario 5: 10' x 6' Triple Box Culvert at West Location & 10' x 6' Double Box Culvert at East Location

Tidal Improvement Scenarios

Flushing Analysis



- Initial concentrations of 1000 (nondimensional units) specific in each waterbody
- 96-hour (4 day) simulation around maximum neap tide conditions
- Time required to diminish concentration by 90% quantified

Tidal Improvement

Flushing Analysis Results



Scenario 1: Triple 10' x 10' box culverts

| Scenario | Area | Time to Dissipate 90% of Concentration (hrs.) | Description | |
|------------|---------|--|-------------------------------------|--|
| Baseline | Western | 11 hrs. | Existing Conditions (No | |
| Ducomito | Eastern | 27 hrs. | Culverts) | |
| | | | | |
| Scopario 1 | Western | 7.75 hrs. (30% Reduction in Flush Time) | Triple 10' x 10' box outparts | |
| Scenario 1 | Eastern | 13.25 hrs. (51% Reduction in Flush Time) | Triple 10 x 10 box cuivens | |
| | | | | |
| Scopario 2 | Western | 9.5 hrs. (14% Reduction in Flush Time) | Double 10' x 10' box | |
| Scenario 2 | Eastern | 15.75 hrs. (42% Reduction in Flush Time) | culverts | |
| | | | | |
| Soonaria 2 | Western | 7.75 hrs. (30% Reduction in Flush Time) | Triple 10' x 10' box culverts | |
| Scenario 5 | Eastern | 16.25 hrs. (40% Reduction in Flush Time) | Double 10' x 10' box culverts | |
| | | | | |
| Scepario 4 | Western | 7.5 hrs. (32% Reduction in Flush Time) | Triple 10' x 8' box culverts | |
| Scenario 4 | Eastern | 16.25 hrs. (40% Reduction in Flush Time) | Double 10' x 8' box culverts | |
| | | | | |
| Scenaria 5 | Western | 8.0 hrs. (27% Reduction in Flush Time) | Triple 10' x 6' box culverts | |
| Scenario 5 | Eastern | 16.25 hrs. (40% Reduction in Flush Time) | Double 10' x 6' box culverts | |

Tidal Improvement

Structure Self-Flushing Hydraulics

- Impoundment of sediment and other materials can decrease hydraulic performance and lead to increased maintenance costs.
- Shear stress trough structures is calculated and compared to recommended values from the literature to evaluate self-flushing capability.
- Shear stress values between 3-4 N/m² are generally sufficient to clear storm sewers per (Yao, 1974).



| Scenario | Western Culvert Shear Stress Percentiles (N/m²) | | | Eastern Culvert Shear Stress Percentiles (N/m²) | | |
|----------|--|------------------|------------------|--|------------------|------------------|
| | 25 th | 50 th | 95 th | 25 th | 50 th | 95 th |
| 1 | 3.91 | 9.62 | 24.10 | 2.17 | 4.94 | 11.31 |
| 2 | 5.09 | 11.90 | 25.60 | 2.66 | 5.73 | 12.24 |
| 3 | 4.96 | 11.43 | 35.09 | 2.94 | 6.22 | 12.59 |
| 4 | 5.01 | 12.12 | 35.03 | 2.94 | 6.22 | 12.59 |
| 5 | 4.96 | 11.39 | 35.09 | 2.94 | 6.23 | 12.61 |

Tidal Improvement

Sedimentation Patterns

- Shear stresses induced by each alternative were developed.
- Shear stresses were related to sediment classifications based on critical bed shear stress values (see USGS Scientific Investigations Report 2008-5093 for more details).



| Particle Classification Name | ticle Classification Name Ranges of Particle Diameters (mm) | | Critical Bed Shear Stress (Tc) (N/m²) | |
|------------------------------|--|----------------------|--|--|
| Very Coarse Sand | 1.0 - 2.0 | 0.029 - 0.039 | 0.47 - 1.30 | |
| Coarse Sand | 0.5 – 1.0 | 0.033 - 0.029 | 0.27 – 0.47 | |
| Medium Sand | 0.25 - 0.50 | 0.048 - 0.033 | 0.194 – 0.27 | |
| Fine Sand | 0.125 – 0.25 | 0.072 - 0.048 | 0.145 – 0.194 | |
| Very Fine Sand | 0.0625 - 0.125 | 0.109 - 0.072 | 0.110 - 0.145 | |
| Coarse Silt | 0.0310 - 0.0625 | 0.165 - 0.109 | 0.0826 - 0.110 | |
| Medium Silt | 0.0156 - 0.0310 | 0.25 - 0 .165 | 0.0630 - 0.0826 | |
| Fine Silt | 0.0078 - 0.0156 | 0.3 - 0.25 | 0.0378 - 0.0630 | |

Conclusion and Path Forward

• Scenario 4 is recommended as the most advantageous alternative and should be progresses through the design phase. This alternative is summarized below:

| Scenario | Number o Struc | Number of Culvert Structures | | Length of Culvert Structures (ft) | | Structure Dimensions (Width x Height) | | Inverts (ft, NAVD88) | |
|----------|-------------------|---------------------------------|------|--------------------------------------|--------|--|------|----------------------|--|
| # | East | West | East | West | East | West | East | West | |
| 4 | 2 | 3 | 260 | 200 | 10'x8' | 10'x8' | -3.4 | -4.2 | |

- Anticipated Project Schedule/Milestones:
 - 30% Design Submitted 01/31/2023
 - 60% Design 06/30/2024
 - Permitting % Final Design 02/28/2025
 - Construction Dependent on acquiring funding.



***** Thank You

